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(19)

Europäisches Patentamt  
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Office européen des brevets



(11)

**EP 0 796 666 B1**

(12)

**EUROPEAN PATENT SPECIFICATION**

(45) Date of publication and mention  
of the grant of the patent:  
05.06.2002 Bulletin 2002/23

(51) Int Cl.7: **B05C 5/00, G03C 1/74**(21) Application number: **97301812.0**(22) Date of filing: **18.03.1997****(54) Light-sensitive material production method**

Verfahren zur Erzeugung von lichtempfindlichem Material

Méthode de production de matériau photosensible

(84) Designated Contracting States:  
**CH DE FR LI**

(30) Priority: **21.03.1996 JP 6441796**

(43) Date of publication of application:  
**24.09.1997 Bulletin 1997/39**

(73) Proprietor: **KONICA CORPORATION**  
**Tokyo (JP)**

(72) Inventors:  
• **Kondo, Yoshikazu**  
**Hino-shi, Tokyo (JP)**

• **Fukazawa, Koji**  
**Hino-shi, Tokyo (JP)**  
• **Nishiwaki, Akira**  
**Hino-shi, Tokyo (JP)**

(74) Representative:  
**Simpson, Alison Elizabeth Fraser et al**  
**Urquhart-Dykes & Lord,**  
**30 Welbeck Street**  
**London W1G 8ER (GB)**

(56) References cited:  
**EP-A- 0 537 086**

**EP 0 796 666 B1**

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**Description****BACKGROUND OF THE INVENTION**

[0001] The present invention relates to a technology to stabilize a curtain coater employing a curtain coating method, and in particular, to a technology to form a curtain layer stably.

[0002] There has been known a curtain coating method wherein a coating solution flowing down along a slide surface of a coater die in a form of a uniform layer is caused to fall from a tip of a die lip of the coater die to be formed into a thin curtain layer of coating solution which is, then, put continuously on a web of a long support while the support is running at a certain high speed for coating. In a coating apparatus manufacturing a light-sensitive material by the use of the curtain coating method mentioned above, it is very important that a curtain layer is formed in a stable manner. It has been cleared that a teapot phenomenon is remarkable, and that phenomenon sometimes caused a curtain layer not to be formed at a bottom end portion of an edge guide (skipped curtain layer) especially in a system wherein a quantity of a coating solution is large. The teapot phenomenon is one wherein with regard to a coating solution which flows down along the slide surface and is just about to fall from the tip of a die lip, a curtain layer does not fall in the vertical direction due to a flow speed of coating solution varying at each point in the direction of a flowing layer thickness, but it falls while it is curved toward the die. Various inventions which will be stated below have been achieved, for improving the skipped curtain layer mentioned above.

[0003] Namely, Japanese Patent Publication Open to Public Inspection No. 99668/1989 (hereinafter referred to as Japanese Patent O.P.I. Publication) discloses a means to strengthen and stabilize a curtain layer by causing side solutions to flow additionally on end portions at both sides for improving the foregoing by preventing the skipped curtain layer. In this means, however, the side solution is accumulated on each end portion intensively, resulting in an excessive thick layer on each of both sides, although the curtain layer is not skipped.

[0004] For the intent of inhibiting the increase in a layer thickness on each side, a thick layer portion on an end portion of a curtain layer is removed through attraction, as disclosed in Japanese Patent O.P.I. Publication Nos. 477/1986 and 233954/1994.

[0005] In Japanese Patent O.P.I. Publication No. 57734/1976, a curtain layer is stabilized by the use of a flat plate type edge guide. However, even this method can not solve the phenomenon of thick layers at both edges.

[0006] European Patent Application 0 537 086 A1 shows a method of coating a substrate, comprising the steps of:

discharging coating solution from a coater die;

forming a curtain layer of coating solution by causing said coating solution to fall from a die lip of said coater die;

wherein said curtain layer is formed with an edge guide by causing an edge of said curtain layer to contact said edge guide, a shape of a section through said edge guide from a top end of said edge guide to a bottom end of said edge guide being straight, and

coating a support with said coating solution by conveying said support at the downstream end of said curtain layer.

(Problems to be solved by the invention)

[0007] In the case of the means to strengthen and stabilize a curtain layer by causing side solutions to flow on edge portions of both sides as stated above, side solutions are accumulated intensively at edge portions on both sides of a coating surface, resulting in increased layer thickness at both sides which applies greater load on a drying process.

[0008] When taking a means of attraction on both sides as stated above for solving the problem mentioned above, an expense for installation of facilities and a load for maintenance expense are increased, and a cost of coating solutions equivalent to those removed at end portions is also increased.

[0009] Further, separately from the foregoing, when using the flat plate type edge guide, it stabilizes a curtain layer no doubt, but a layer thickness on the side of a curtain layer is increased to create a thick layer because an area of contact between the flat plate type edge guide and a coating solution is increased, which results in greater load on a drying process and in reduction in an effective width for a product.

[0010] Namely, as far as the inventions mentioned above are concerned, a curtain layer can be stabilized to a certain extent, but an area of contact between a coating solution and an edge guide is increased and edge portions are made to be uneven accordingly, in any case of the inventions mentioned above. Therefore, a load for drying thick layer portions is caused and sufficient uniform coating necessary for products can not be obtained, and in spite of the insufficient effect, installation of facilities and actions for the effect are needed, which has resulted in an increase in expenses. Accordingly, it has been required a method wherein the relation of the state of contact between an edge guide and a coating solution is investigated and a curtain layer can be stabilized.

[0011] An object of the invention is to provide a curtain coater wherein the problems in prior art mentioned above have been solved, and it is possible to manufacture a material having high quality and high yield while applying low load on a drying process, by coating with extremely uniform edge portions while forming a stable curtain layer through a curtain coating method.

**[0012]** The object mentioned above can be attained by either one of the following methods (1) - (4).

(1) A method of coating a substrate, comprising the steps of:

discharging coating solution from a coater die; forming a curtain layer of coating solution by causing said coating solution to fall from a die lip of said coater die;

wherein said curtain layer is formed with an edge guide by causing an edge of said curtain layer to contact said edge guide, a shape of a section through said edge guide from a top end of said edge guide to a bottom end of said edge guide, where said edge guide contacts said curtain layer, is round, and said edge guide is formed along a cross sectional shape of a curtain layer which is formed if said coating solution falls from said die lip without said edge guide; and coating a support with said coating solution by conveying said support at the downstream end of said curtain layer.

(2) The method described in Item No. (1), in which discharging amount of the coating solution from the coater die is not less than 2 cc/sec./cm.

(3) The method described in Item No. (3), in which the cross sectional shape is the teapot phenomenon shape.

(4) the method described in Item No. (1), in which a distance between the axial center of the edge guide and the longitudinal center at the downstream end of the curtain layer, which is formed when the coating solution is fallen from the die lip without the edge guide, is not more than  $\pm 4$  mm in a direction perpendicular to the longitudinal direction of the curtain layer.

**[0013]** Namely, the inventors of the invention confirmed through experiments, after studying an improvement of a curtain coater in accordance with the object mentioned above, that the teapot phenomenon, in particular, becomes remarkable in the system where the total quantity of coating solution to be supplied is 2 cc/sec./cm or more and that the teapot phenomenon impedes formation of a curtain layer. Further, as a result of the study wherein an edge guide formed to be curved to follow each teapot phenomenon shape was prepared for each of the systems having different flow rates, it was cleared that stability of a curtain layer is improved much more by the curved edge guide than by an uncurved, straight and bar-shaped edge guide arranged vertically. In addition, even in the case of the straight and bar-shaped edge guide, it was found that stability of a curtain layer can be improved when the edge guide is arranged to be tilted so that the bottom end of the edge guide may be shifted toward a coater die to follow the teapot position. Since these methods can stabilize a curtain layer

while keeping an area of contact between an edge guide and a coating solution to the minimum, they are considered to be far better than conventional methods employing an edge guide of a flat plate type of side coating solutions, on the point that edge portions of coated products are made uniform. Incidentally, these effects have been confirmed also by a shape (e.g., a flat plate type, a round type) of a section of the edge guide positioned on the side where the edge guide comes in contact with a curtain layer.

**[0014]** In curtain coating, it is very important that curtain layers are formed in a stable manner. Accordingly, there have been applied many inventions concerning the matter mentioned above.

**[0015]** On the other hand, however, there exist various needs for an improvement in yield and for cost reduction, and therefore, edge portions of a curtain layer must be made uniform to the utmost extent. Figs. 7 (A) through 7 (C) represent sectional views for edge guide 6 and curtain layer 7. Each of Figs. 7 (A) - 7 (C) shows an example wherein each edge guide is arranged to hang down vertically from a lip portion. With regard to each edge guide, a curtain layer can be formed no doubt more stably in (C) than in (A) and (B). However, edge portions of the coated layer are not uniform, which makes it impossible to secure a sufficient effective width for a product. In the case of (A) and (B), on the other hand, it is difficult to form a curtain layer in a stable manner, and the thinner an edge guide bar is in terms of thickness, the smaller an area of contact with liquid is, resulting in a more remarkable tendency toward the phenomena mentioned above. It is therefore necessary to have a technology which makes it possible to form a curtain layer in a stable manner even when the edge guide used is made thin to the utmost extent.

**[0016]** In the invention this time, therefore, a layer thickness on the edge portion can be uniform provided that an edge guide is within a range of 1.0 - 6.0 mm, and even when a thickness of the edge guide is lowered to a value (approx. 1 mm) equivalent mostly to the thickness of a layer flowing down to be a curtain layer, a curtain layer can be formed stably.

#### BRIEF DESCRIPTION OF THE DRAWINGS

**[0017]** Fig. 1 is a perspective view of a curtain layer forming section in a curtain coater of the invention.

**[0018]** Fig. 2 is a side view showing the relation between various edge guides and curtain layer forming.

**[0019]** Fig. 3 is a perspective view showing the relation between various edge guides and curtain layer forming.

**[0020]** Fig. 4 represents a graph showing the relation between deviation width of teapot  $\alpha$  and stability of a curtain layer.

**[0021]** Fig. 5 represents a graph showing the relation between deviation width of teapot  $\alpha$  and a rate of thick layer on edge area.

[0022] Fig. 6 represents a graph showing the relation between deviation width of teapot  $\alpha$  and stability of a curtain layer effected when various edge guides of an oblique type are used.

[0023] Figs. 7(A) through 7(C) each represents a cross sectional view of a conventional edge guide and a curtain layer formed on the conventional edge guide.

## DETAILED DESCRIPTION OF THE INVENTION

[0024] An embodiment of the invention will be explained as follows, referring to a perspective view in Fig. 1. Long support 2 is wound around back roller 1 so that the support can be conveyed in the arrowed direction at a constant speed. Coater die 3 is provided to be diagonally to the upper portion of the back roller 1, and plural layers of coating solutions, including light-sensitive material and discharged from the coater die 3, flow down, while forming their uniform layer thicknesses, along slide surface 4 of the coater die 3 to the tip portion of die lip 5 of the coater die 3 where the plural layers leave the die lip 5 to fall while forming a thin curtain layer. In this case, both sides of the curtain layer are put on support 2 which is running at the constant speed while a uniform layer is being formed and maintained due to dynamic surface tension (DST) generated between edge guide 6 and the curtain layer, thus, continuous coating is achieved. In this case, the DST was measured in accordance with "A New Method of Measuring Dynamic Surface Tension" in Journal of Colloid and Interface Science. Vol.77 No.2 October 1980.

[0025] The edge guide 6 includes a straight bar-shaped one tilted toward coater die 3 as shown in Fig. 2 (b) and a bar-shaped one curved to be a shape of a circular arc whose average radius is 200 - 250 mm as shown in Fig. 2 (c). Incidentally, what is shown in Fig. 2 (a) is a conventional one that is a straight and bar-shaped edge guide arranged vertically.

[0026] There will be explained as follows concerning noticeable effects in terms of the state of the finishing of coating exhibited in the case wherein the edge guides shown in Figs. 2 (b) and 2 (c) were used, compared with an occasion where a conventional edge guide shown in Fig. 2 (a) was used.

## EXAMPLES

### Example 1

#### Fundamental conditions of the experiment

#### [0027]

Composition of each coating solution: Aqueous solution of 7% gelatin adjusted to 30 cp by thickening agents  
Layer structure: 2 - 10 layers  
Curtain height: 30 - 300 mm

Coating speed: 100 - 400 m/min.

Curtain layer width: 300 mm

#### Measurement of teapot amount

[0028] As shown in a perspective view of Fig. 3, a distance between a central portion in the width of a curtain layer on its bottom end and a point of contact between the curtain layer and an edge guide at both ends in the direction that is perpendicular to the lateral direction of the curtain layer and is horizontal was measured as deviation width of teapot  $\alpha$  (mm). In the measurement, it was assumed that  $\alpha$  takes a plus sign when the central portion on the bottom end of the curtain layer is positioned between a point of contact for both the curtain layer and the edge guide at both ends and coater die 3, while  $\alpha$  takes a minus sign when that central portion is positioned between a point of contact for both the curtain layer and the edge guide at both ends and back roller 1. Edge guide used: (shown in Figs. 2 (a), 2 (b) and 2 (c))

(a) straight and bar-shaped edge guide provided vertically: shown by ▲

(b) straight and bar-shaped edge guide provided obliquely: shown by ●

(c) Edge guide in a shape following teapot phenomenon: shown by ■

#### Measurement of a rate of thick layer on edge area

[0029] Dried thick layer area A and normal area B both of a coated product were measured, and  $A/B \times 100$  was calculated for obtaining the rate of thick layer on edge area.

evaluation

A: Possible to coat

B: Curtain layer breakage after start of coating

C: Curtain layer breakage

[0030] First, the relation between deviation width of teapot  $\alpha$  and stability of a curtain layer is like one shown in a graph of Fig. 4.

[0031] As is clear from Fig. 4, it is understood that when a bar-shaped edge guide of an oblique type and an edge guide following a teapot phenomenon are used, stability of a curtain layer can be obtained when an absolute value of  $\alpha$  is not more than 4 mm, but the curtain layer becomes unstable when an absolute value of  $\alpha$  is not less than 4 mm. However, it is also understood that the curtain layer becomes unstable even when an absolute value of  $\alpha$  is not more than 4 mm, if a bar-shaped edge guide of a vertical type is used.

[0032] Further, the relation between deviation width of teapot  $\alpha$  and a rate of thick layer on edge area of a curtain layer comes to one like a graph shown in Fig. 5.

[0033] A graph in Fig. 5 makes the following clear. when a bar-shaped edge guide of an oblique type and an edge guide following a teapot phenomenon are used, the rate of thick layer on edge area of a curtain layer is about 130%, which means that the thick layer is improved remarkably. The rate of thick layer on edge area at such level does not cause any load for drying, and it is considered to be in a range allowable in terms of quality as a product. However, when a conventional edge guide of a flat plate type is used, the rate of thick layer on edge area of a curtain layer goes up to about 180%, which causes heavy load for drying, and there is presented a phenomenon that a conveyance path in a drying section is contaminated by insufficient drying, and product quality in coating is extremely impeded.

[0034] In the example shown in a graph of Fig. 6, the relation between deviation width of teapot  $\alpha$  and stability of a curtain layer is plotted under the same conditions as in the foregoing except that a round bar of 6 mm in diameter and that of 2 mm in diameter as well as a square pillar of 6 mm in section side and that of 2 mm in section side are used as a bar-shaped edge guide of an oblique type. Even in this example, no difference was observed in 4 kinds of edge guides each having different shape and dimension, and results in this case were mostly the same as those in the example shown in the graph of Fig. 4.

[0035] The invention has made it possible to provide a curtain coater capable of coating on both edge areas extremely uniformly while forming a stable curtain layer, and also capable of manufacturing light-sensitive materials which are of high quality, high yield and low load for drying.

#### Claims

1. A method of coating a substrate, comprising the steps of:

discharging coating solution from a coater die; forming a curtain layer of coating solution by causing said coating solution to fall from a die lip of said coater die; wherein said curtain layer is formed with an edge guide by causing an edge of said curtain layer to contact said edge guide, a shape of a section through said edge guide from a top end of said edge guide to a bottom end of said edge guide, where said edge guide contacts said curtain layer, is round, and said edge guide is formed along a cross sectional shape of a curtain layer which is formed if said coating solution falls from said die lip without said edge guide; and coating a support with said coating solution by conveying said support at the downstream end of said curtain layer.

2. The method of claim 1, wherein discharging amount of said coating solution from said coater die is not less than 2 cc/sec./cm.
3. The method of claim 1, wherein said cross sectional shape is the teapot phenomenon shape.
4. The method of claim 1, wherein a distance between the axial center of said edge guide and the longitudinal center at the downstream end of said curtain layer, which is formed if said coating solution falls from said die lip without said edge guide, is not more than  $\pm 4$  mm in a direction perpendicular to the longitudinal direction of said curtain layer.
5. The method of claim 1, wherein said coating solution comprises a light-sensitive material.

#### Patentansprüche

1. Verfahren zum Beschichten eines Substrats, mit folgenden Schritten:

Austragen einer Beschichtungslösung aus einer Beschichterform;  
Formen einer Beschichtungslösungs-Vorhangschicht, indem bewirkt wird, dass die Beschichtungslösung von einer Formlippe der Beschichterform herabfällt;

wobei die Vorhangschicht mit einer Randführung gebildet wird, indem ein Rand der Vorhangschicht mit der Randführung in Kontakt gebracht wird, wobei eine Form eines Querschnitts durch die Randführung von einem oberen Ende der Randführung zu einem unteren Ende der Randführung, an der die Randführung mit der Vorhangschicht in Kontakt steht, rund ist, und die Randführung entlang einer Querschnittsform einer Vorhangschicht ausgebildet wird, welche gebildet wird, wenn die Beschichtungslösung ohne die Randführung von der Formlippe herabfällt; und

Beschichten eines Trägers mit der Beschichtungslösung durch Bewegen bzw. Transportieren des Trägers am stromabwärtigen Ende der Vorhangschicht.

2. Verfahren nach Anspruch 1, wobei die Austragsmenge der Beschichtungslösung aus der Beschichterform nicht weniger als 2 cc/sec/cm beträgt.
3. Verfahren nach Anspruch 1, wobei die Querschnittsform eine Teekannen-Erscheinungsform aufweist.
4. Verfahren nach Anspruch 1, wobei ein Abstand zwi-

schen dem axialen Zentrum der Randführung und dem longitudinalen Zentrum am stromabwärtigen Ende der Vorhangschicht, die gebildet wird, wenn die Beschichtungslösung ohne die Randführung von der Formlippe herabfällt, nicht mehr als  $\pm 4$  mm in einer zur Längsrichtung der Vorhangschicht senkrechten Richtung beträgt.

5. Verfahren nach Anspruch 1, wobei die Beschichtungslösung ein lichtempfindliches Material umfasst.

dans une direction perpendiculaire à la direction longitudinale de ladite couche à rideau.

5. Le procédé selon la revendication 1, dans laquelle ladite solution de revêtement comprend une substance photosensible.

## Revendications

1. Un procédé de recouvrement d'un substrat comprenant les étapes dans lesquelles :

- on décharge une solution de revêtement d'une buse d'applicateur ;
- on forme une couche en nappe ou rideau de solution de revêtement en faisant descendre ladite solution de revêtement de la lèvre de la buse de ladite buse d'applicateur ;

dans laquelle la forme de ladite couche ou rideau avec un coude latéral, amenant une bordure de ladite couche en rideau en contact avec ledit guide latéral, une forme d'une section dans ledit guide latéral du sommet dudit guide latéral à l'extrémité inférieure dudit guide latéral, dans lequel ledit guide latéral vient en contact avec ladite couche en rideau, étant ronde, et ledit guide latéral étant formé le long d'une forme en section transversale d'une couche en rideau qui est formée si ladite solution de revêtement descend de ladite lèvre de la buse sans ledit guide latéral ; et

- le recouvrement d'un support avec ladite solution de recouvrement en déplaçant ledit support à l'extrémité aval de ladite couche en rideau.

2. Le procédé selon la revendication 1, dans laquelle la quantité déchargée de ladite solution de revêtement de ladite buse d'applicateur n'est pas inférieure à  $2 \text{ cm}^3/\text{seconde/cm}$ .

3. Le procédé selon la revendication 1, dans laquelle ladite forme de section transversale est de la forme dudit "phénomène de théière".

4. Le procédé selon la revendication 1, dans laquelle la distance entre le centre axial dudit guide latéral et le centre longitudinal à l'extrémité aval de ladite couche en rideau, qui se forme si ladite solution de revêtement tombe de ladite lèvre de la buse sans ledit guide latéral, n'est pas supérieure à  $\pm 4$  mm

FIG. 1

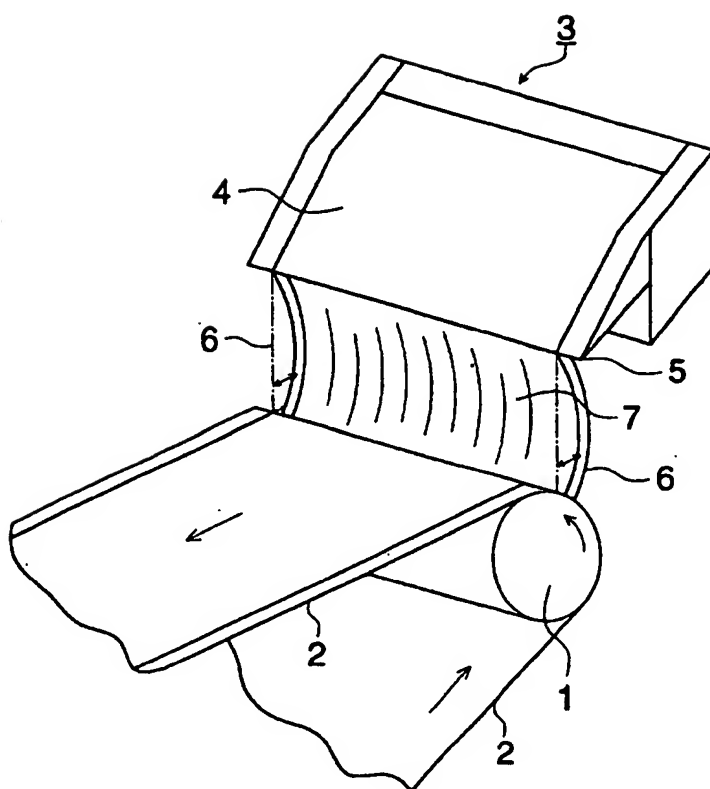


FIG. 2 (a)

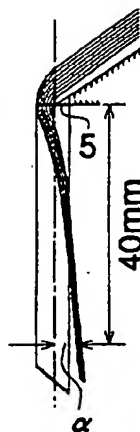


FIG. 2 (b)

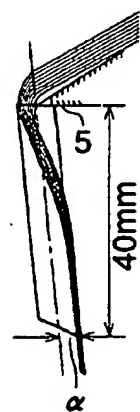


FIG. 2 (c)

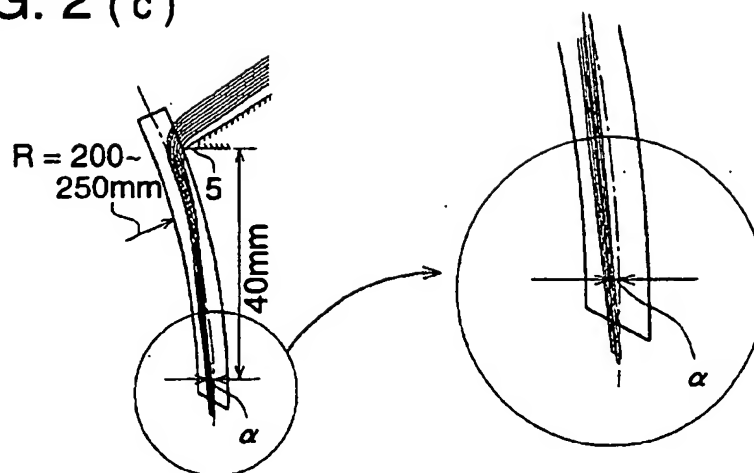




FIG. 3

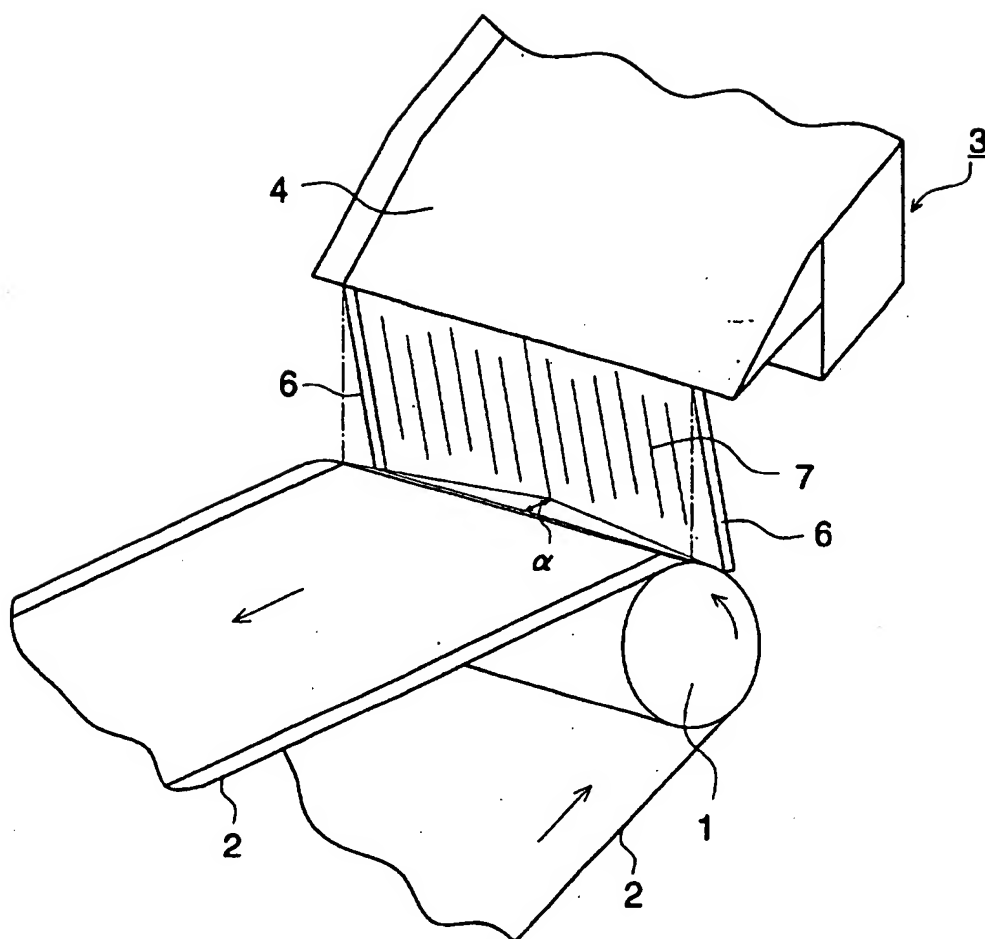


FIG. 4

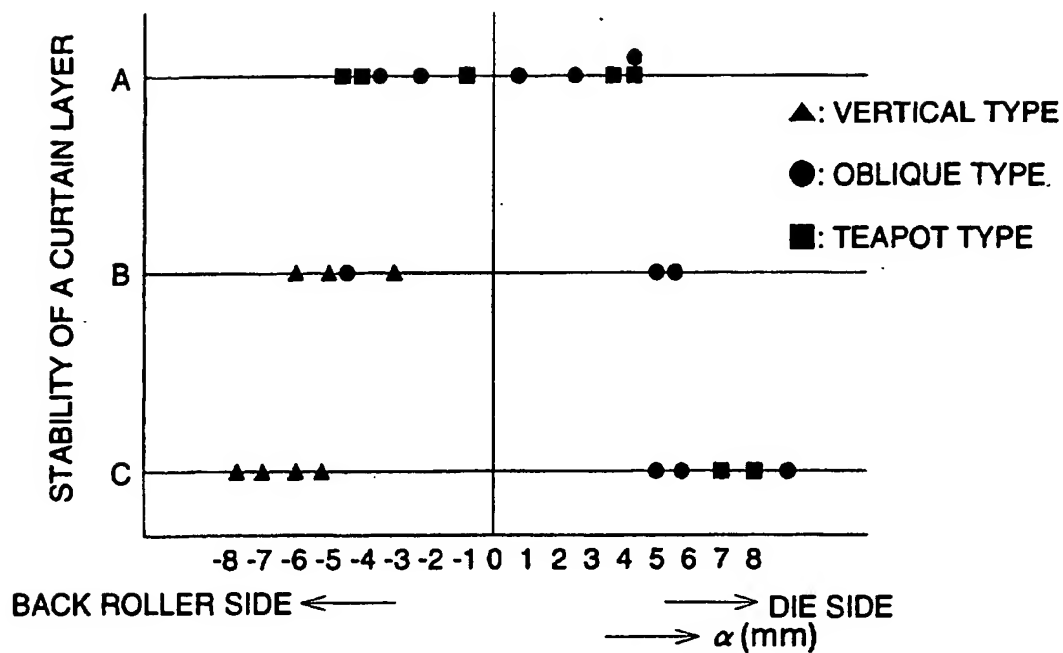


FIG. 5

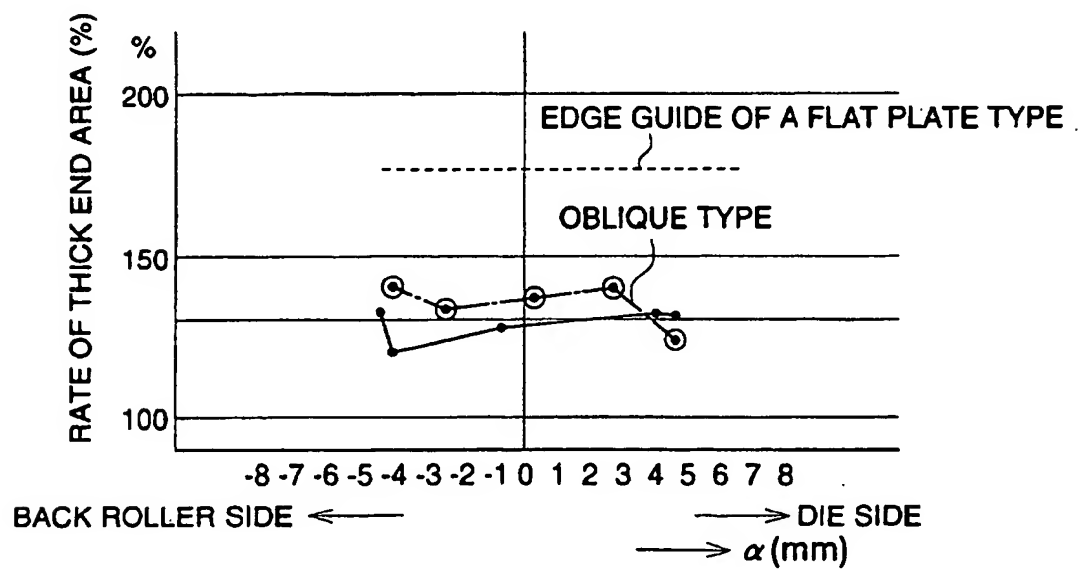


FIG. 6

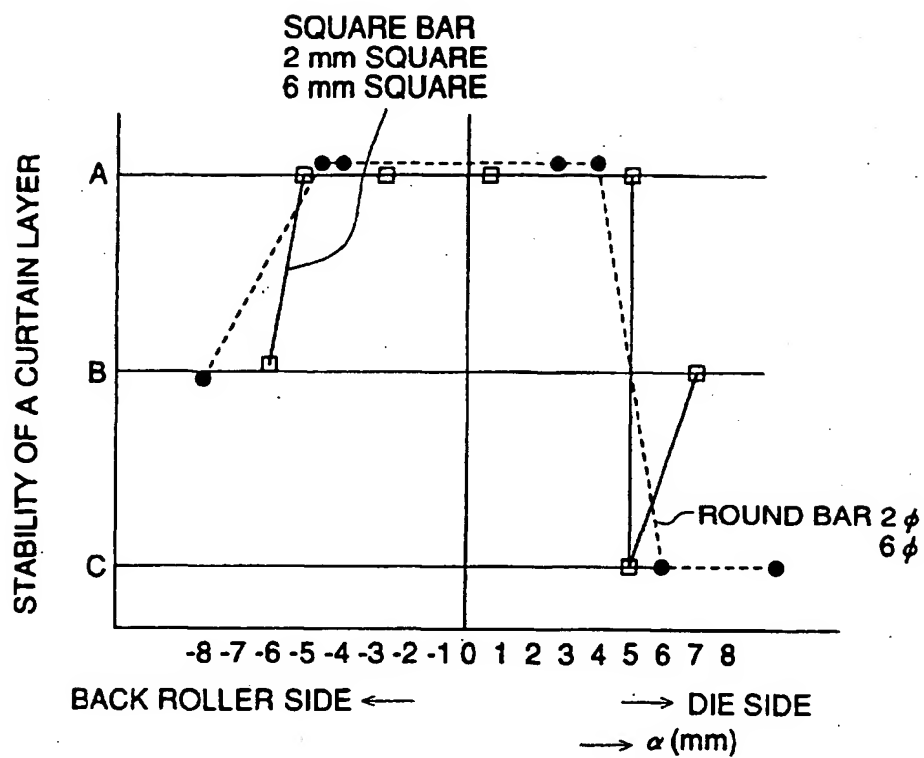


FIG. 7 (A)

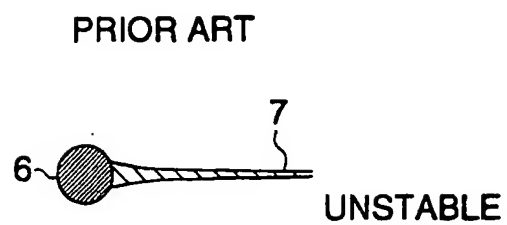


FIG. 7 (B)

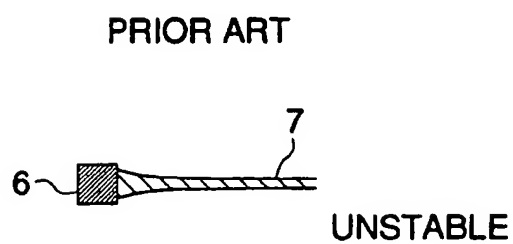


FIG. 7 (C)

